

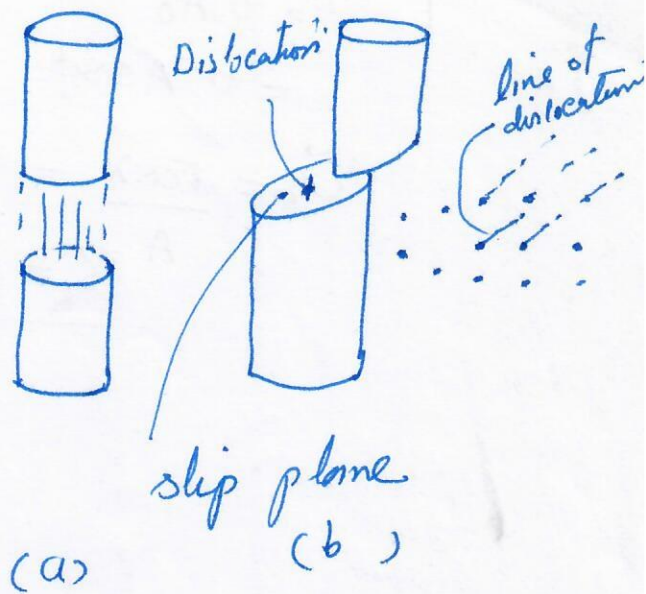
## Significance of Dislocations

Without dislocations

(a), a material will fail by breaking all of the bonds across the surface

As - However when a

dislocation slips (b), bonds are only broken along the line of the dislocation.



### EXAMPLE

A typical dislocation density in soft copper is  $10^6 \text{ cm/cm}^3$ . If the dislocations in 1000g of copper were placed end to end, how many miles of dislocation would be available?

(Normally dislocation density of  $10^6 \text{ cm/cm}^3$  are typical of the soft materials)

the density of copper is  $8.93 \text{ Mg/m}^3$  Mega

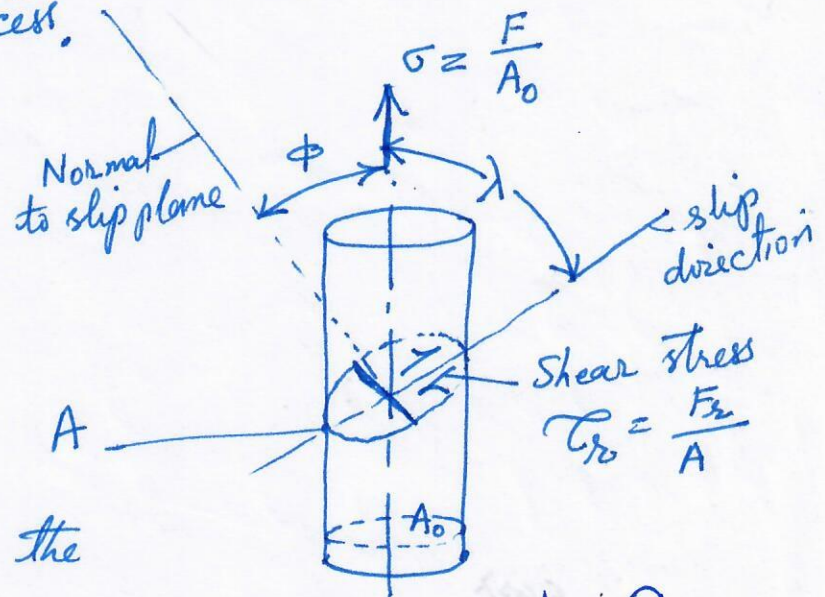
$$\text{Volume of copper} = \frac{1000\text{g}}{8.93\text{g/cm}^3} = 112 \text{ cm}^3$$

$$\begin{aligned} \text{Length} &= (112 \text{ cm}^3) (10^6 \text{ cm} / \text{cm}^3) = 1.12 \times 10^8 \text{ cm} \\ &= \frac{(1.12 \times 10^8 \text{ cm})}{(2.54 \text{ cm} / \text{in.}) (12 \text{ in} / \text{ft}) (5280 \text{ ft} / \text{mile})} \\ &= 696 \text{ miles.} \end{aligned}$$

## SCHMID'S LAW

We can understand the difference in behaviours of metals that have different crystal structures by examining the slip process.

A resolved shear stress  $\tau$  may be produced on a slip system, causing the dislocation to move on the a ~~slip system~~ slip plane in the slip direction.



$$\begin{aligned} \lambda + \phi &= 90 \\ \text{if } \lambda &= 90, \phi = 0 \\ \text{if } \phi &= 90, \lambda = 0 \end{aligned}$$

where  $\tau_s = \frac{F_s}{A}$  = resolved shear stress in the slip direction.

$\sigma = \frac{F}{A_0}$  = unidirectional stress applied to the cylinder.

$$F_s = F \cos \lambda \quad \tau_s = \frac{F \cos \lambda \sin \phi}{A_0 \cos \phi} = \sigma \cos \lambda \sin \phi$$

$A \cos \phi = A_0$

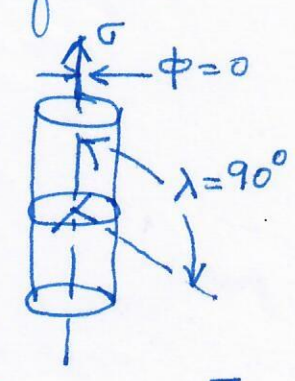
$\lambda \rightarrow$  angle between the slip direction and the applied force

$\phi \rightarrow$  Angle between the normal to the slip plane and the applied force

resolved  
 $A_0 = A \cos \phi$   
 $F_R = F \cos \lambda$   
 $A_0 = A \cos \phi$

Schmid's Law

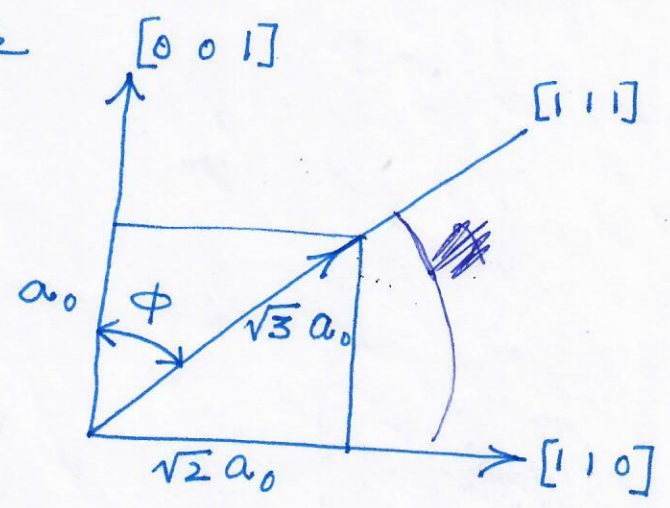
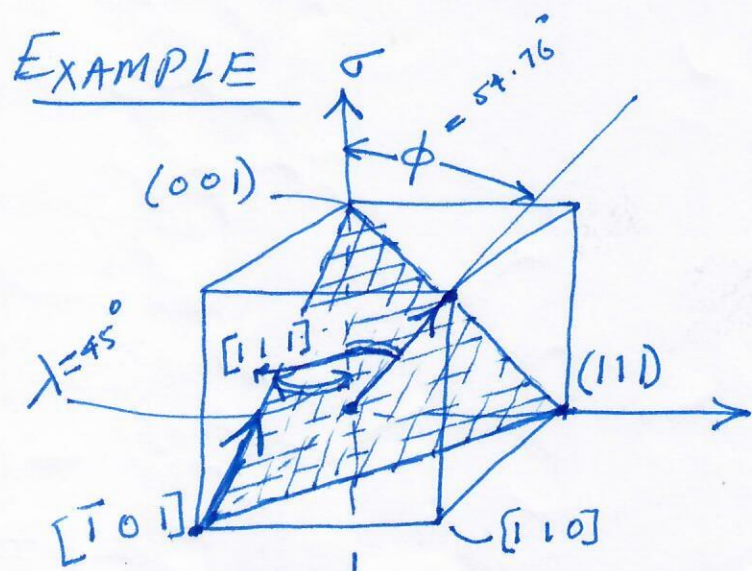
when the slip plane is perpendicular to the applied stress  $\sigma$ , the angle  $\lambda$  is  $90^\circ$  and no shear stress is resolved



$\tau_R = \sigma \cos \phi \cos \lambda$  where  $\tau_R = \frac{F_R}{A}$ ,  $\sigma = \frac{F}{A_0}$

EXAMPLE

If  $\lambda$  or  $\phi$  is  $90^\circ$  no slip will occur



A normal stress  $\sigma$  is applied in the ~~[001]~~  $[001]$  direction of the unit cell. This produces an angle  $\lambda$  of  $45^\circ$  to the  $[100]$  slip direction and an angle  $\phi = 54.76^\circ$  to the

## EXAMPLE

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Calculate the resolved shear stress on the (111)  $[\bar{1}01]$  slip system if a stress of 70 MPa is applied in the  $[001]$  direction of an FCC unit cell.

Solution

From Fig.  $\lambda = 45^\circ$ ,  $\cos \lambda = 0.707$

The normal to the (111) plane must be the  $[111]$  direction. One can find

$$\cos \phi = \frac{1}{\sqrt{3}} = 0.577, \quad \phi = 54.76^\circ$$

$$\begin{aligned}\tau_R &= \sigma \cos \lambda \cos \phi = (70 \text{ MPa})(0.707)(0.577) \\ &= 28.56 \text{ MPa}\end{aligned}$$

Critical resolved shear stress is the

$\tau_{\text{crss}}$  is the <sup>↑ minimum</sup> shear stress required to break enough metallic bonds in order for slip to occur. Thus slip occurs, causing the metal to deform, when the applied stress produces a resolved shear stress that equals the critical resolved shear stress, slip occurs.

$$\tau_R = \tau_{\text{crss}}$$

## EXAMPLE

Consider a slip system in which  $\lambda = 70^\circ$   
 $\phi = 30^\circ$

Solution

Since at 35 MPa slip just starts  
to occur in  $\tau_{crss} = \tau_s$ .

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$$\tau_{crss} = \tau_s \text{ when slip begins}$$

$$\begin{aligned}\tau_{crss} &= \sigma_{crs} \cos \phi = (35 \text{ MPa})(\cos 70^\circ)(\cos 30^\circ) \\ &= 10.37 \text{ MPa}\end{aligned}$$